

Solid Fuel Combustion Research
in the
Energy and Environmental Technology Laboratory
at Brown University

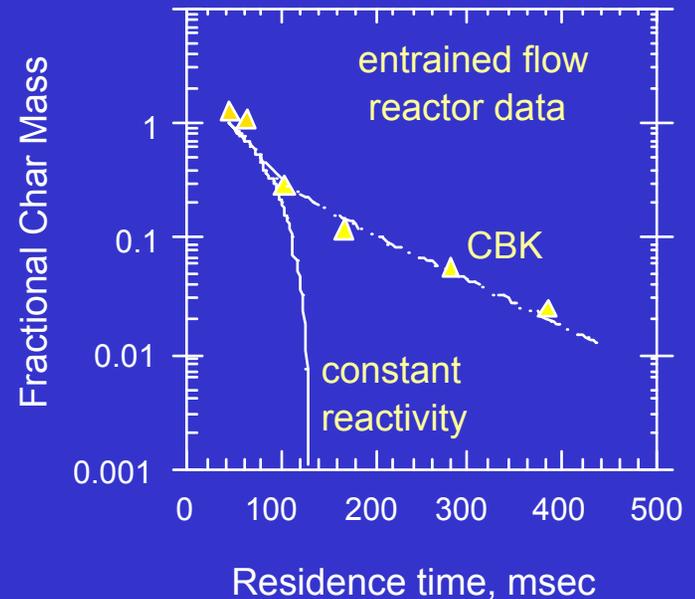
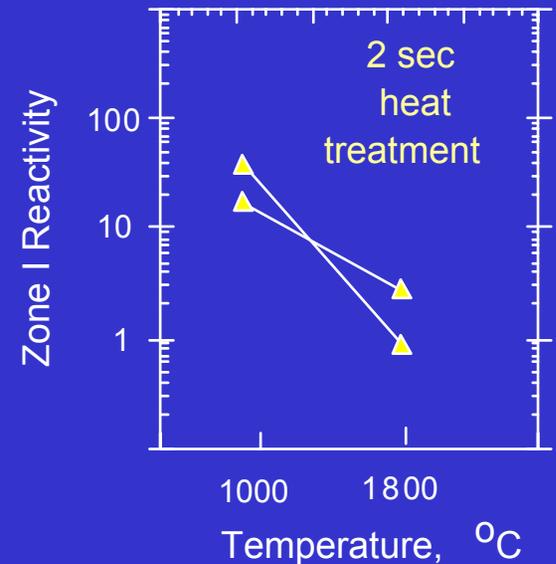
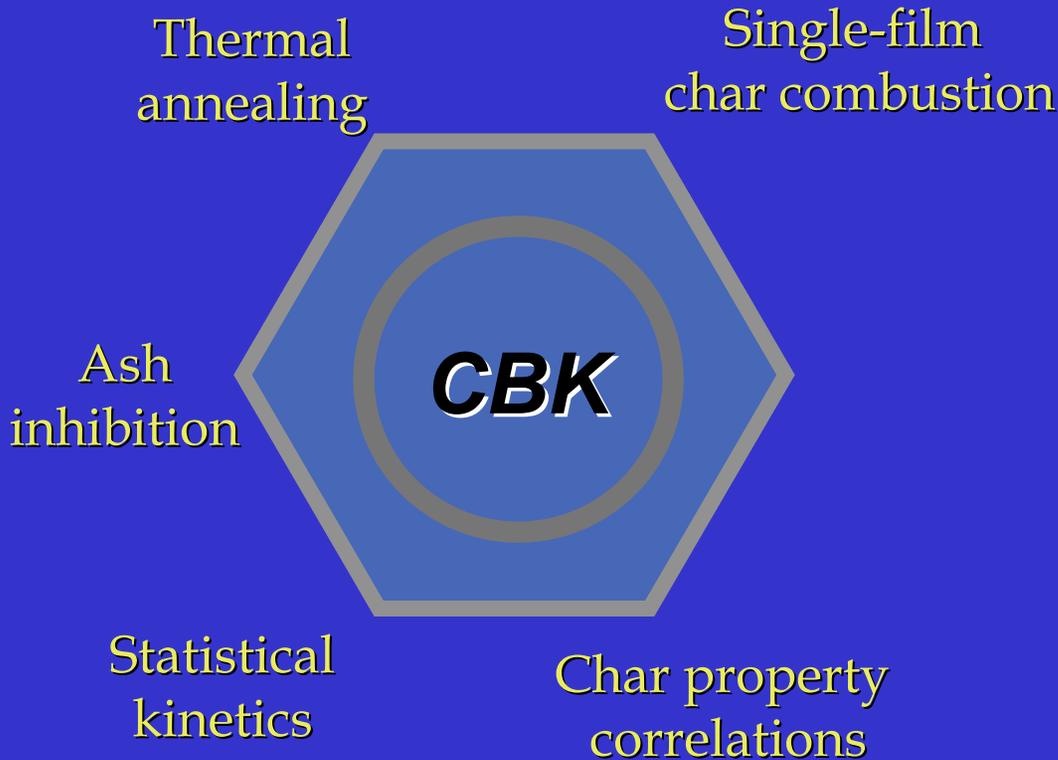
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Division of Engineering, Brown University

*Presented at the NETL Combustion Technology University
Workshop, Columbus, Ohio, August 2003*

Work at Brown led to the CBK model now integrated in *Fluent* and *Glacier* CFD codes

Carbon Burnout Kinetics



New work to extend CBK to high pressure char combustion

Characteristic
Burnout Rate, $R_{BO} = \frac{dm / dt}{m_o}$
(1/burnout time)

In Zone III
(diffusion-limited reaction)

$$R_{BO} = \frac{k_m X_{ox} P d_p^2}{\rho d_p^3} = X_{ox} / \rho d_p^2$$

$$R_{BO} = \frac{X_{ox}}{(\rho d_p^2)_{coal} (1-VM) \omega}$$

In Zone I
(kinetically-limited reaction)

$$R_{BO} = k_{int} P^n$$

derivable from other properties

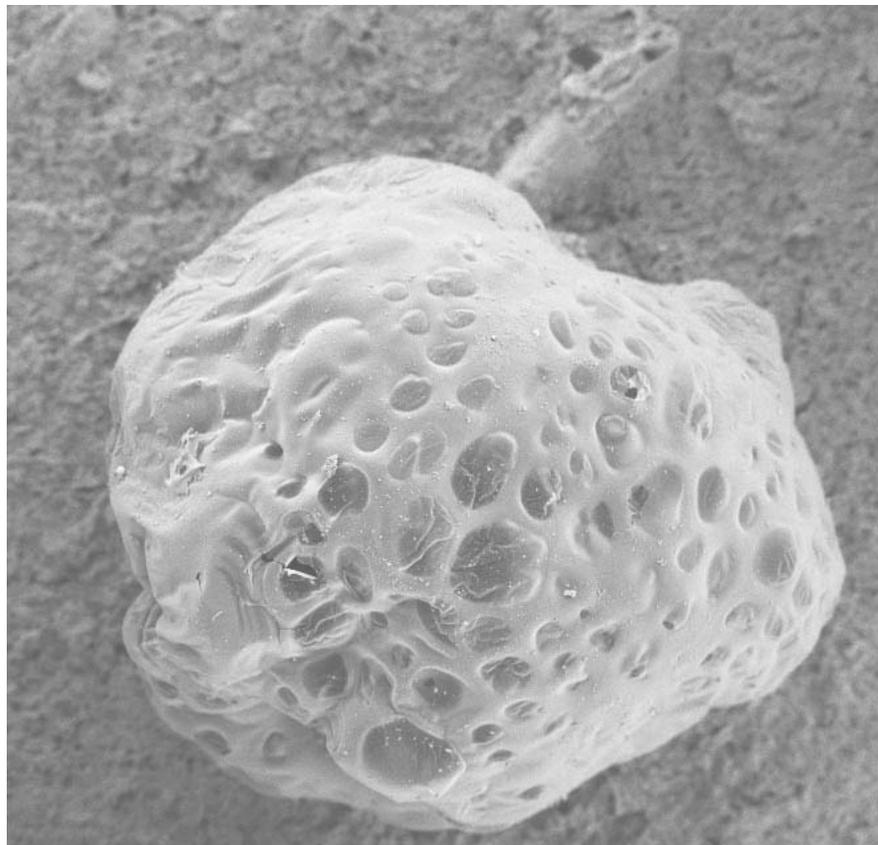
CFD-based models need: VM^* , ω^* , k_{in}^* , n^* , porosity (some models), ρ_{char}

High-Pressure Char Morphology

Illinois#6, 20 atm. O/C: 58%

3 kV e-beam

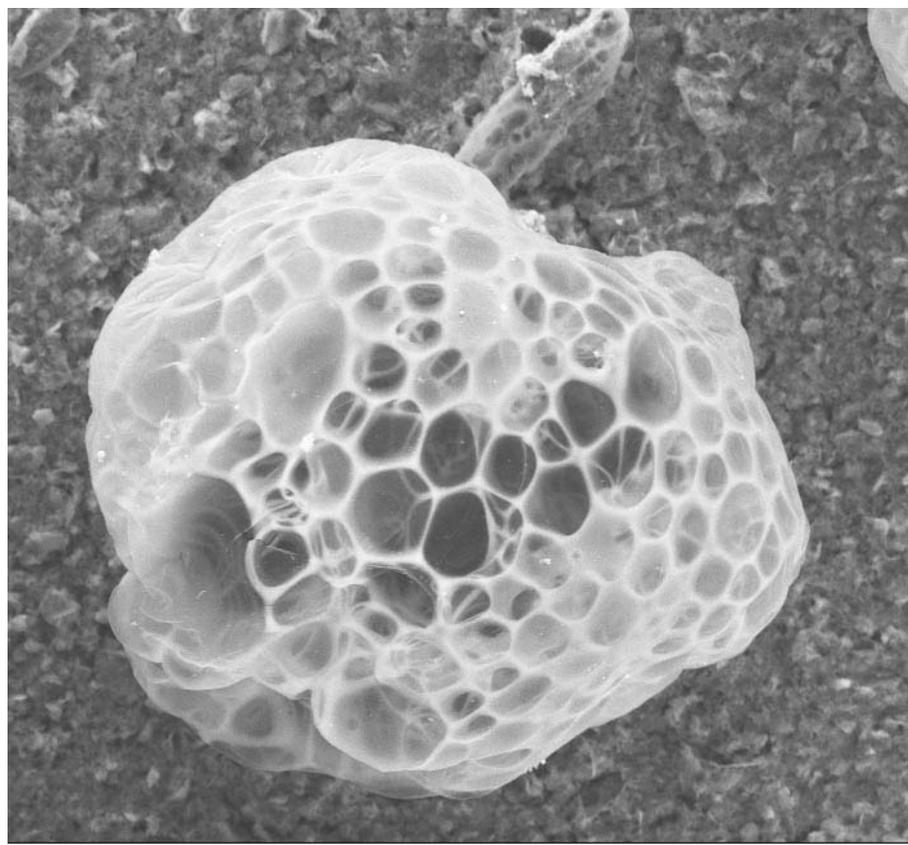
20 kV e-beam



20µm
| |

EHT = 3.07 kV
WD = 8 mm

Signal A = VPSE
Photo No. = 538
Date :6
Time :1



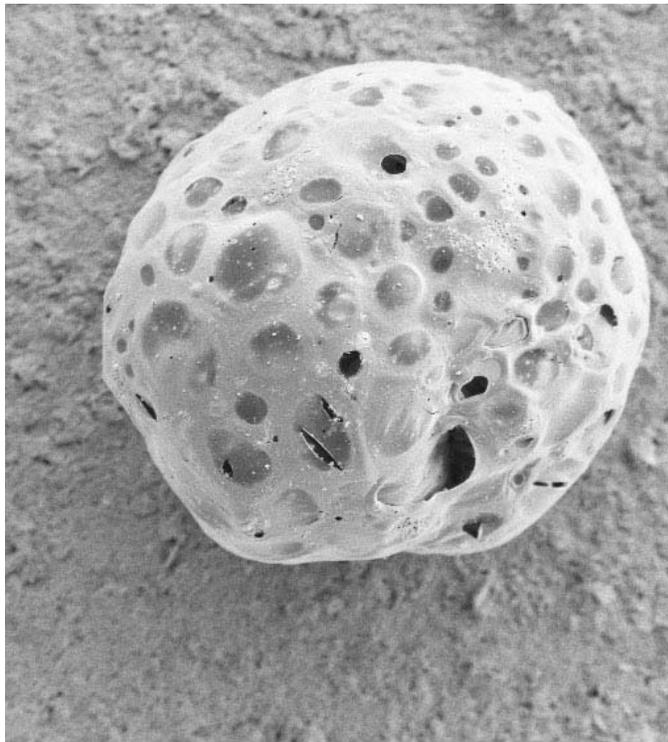
20µm
| |

EHT = 19.96 kV
WD = 8 mm

Signal A = VPSE
Photo No. = 540
Date :6
Time :1

High-Pressure Char Morphology

Pitt. #8, 30 bar, O/Coal 48.6%

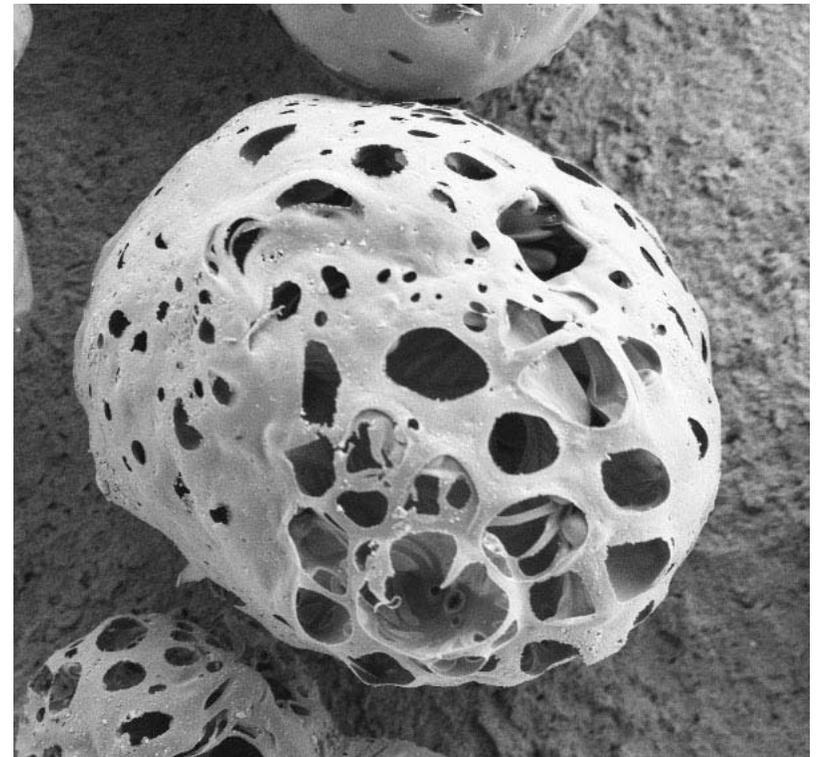


20µm
|-----|

EHT = 3.03 kV
WD = 11 mm

Signal A =
Photo No.

Pitt. #8, 30 bar, O/Coal 103%

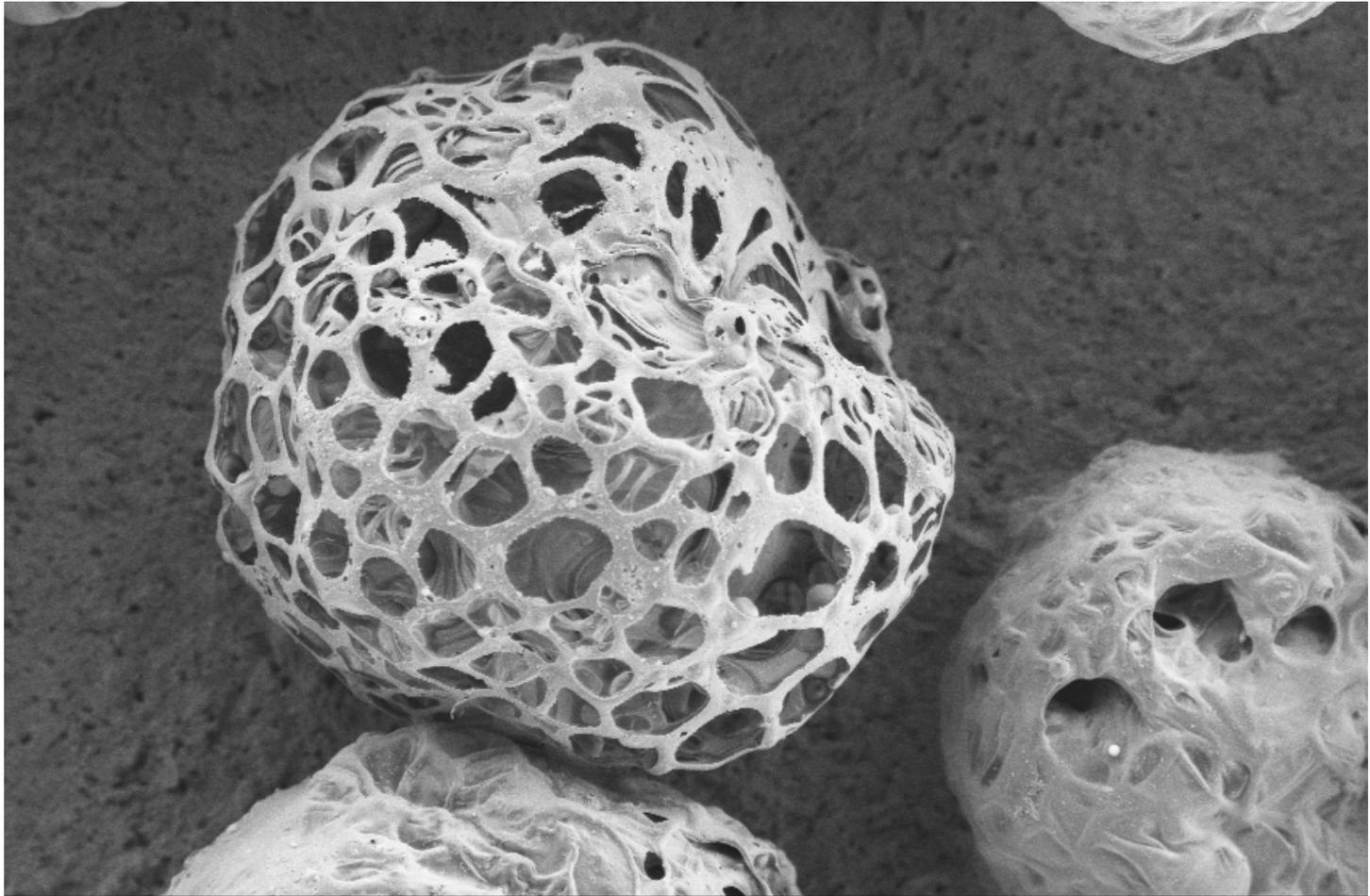


x
20µm
|-----|

EHT = 3.03 kV
WD = 11 mm

Signal A = VPSE
Photo No. = 940

Pittsburgh #8, 10 atm. O/C: 29.8%



20 μ m
|—|

EHT = 3.07 kV
WD = 9 mm

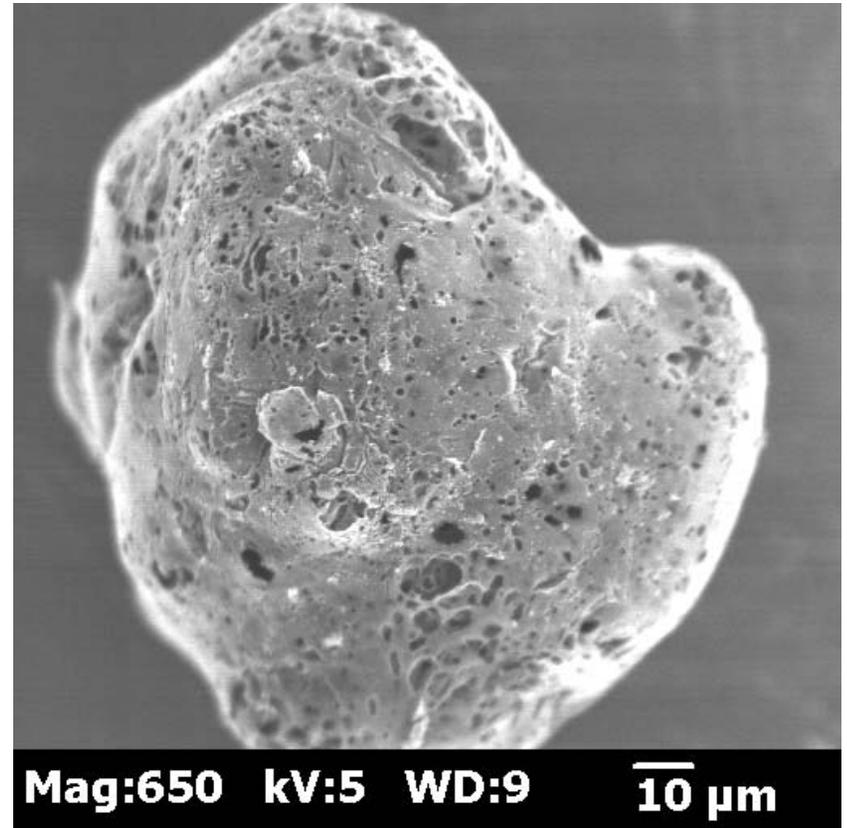
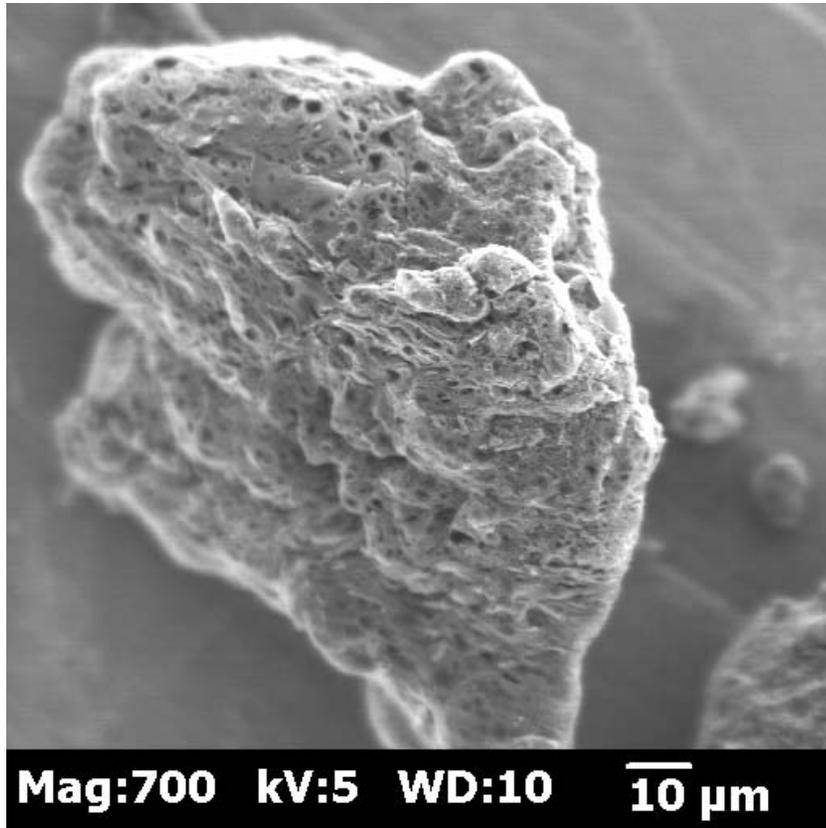
Signal A = VPSE
Photo No. = 659

Date :20 Mar 2003
Time :14:58:29

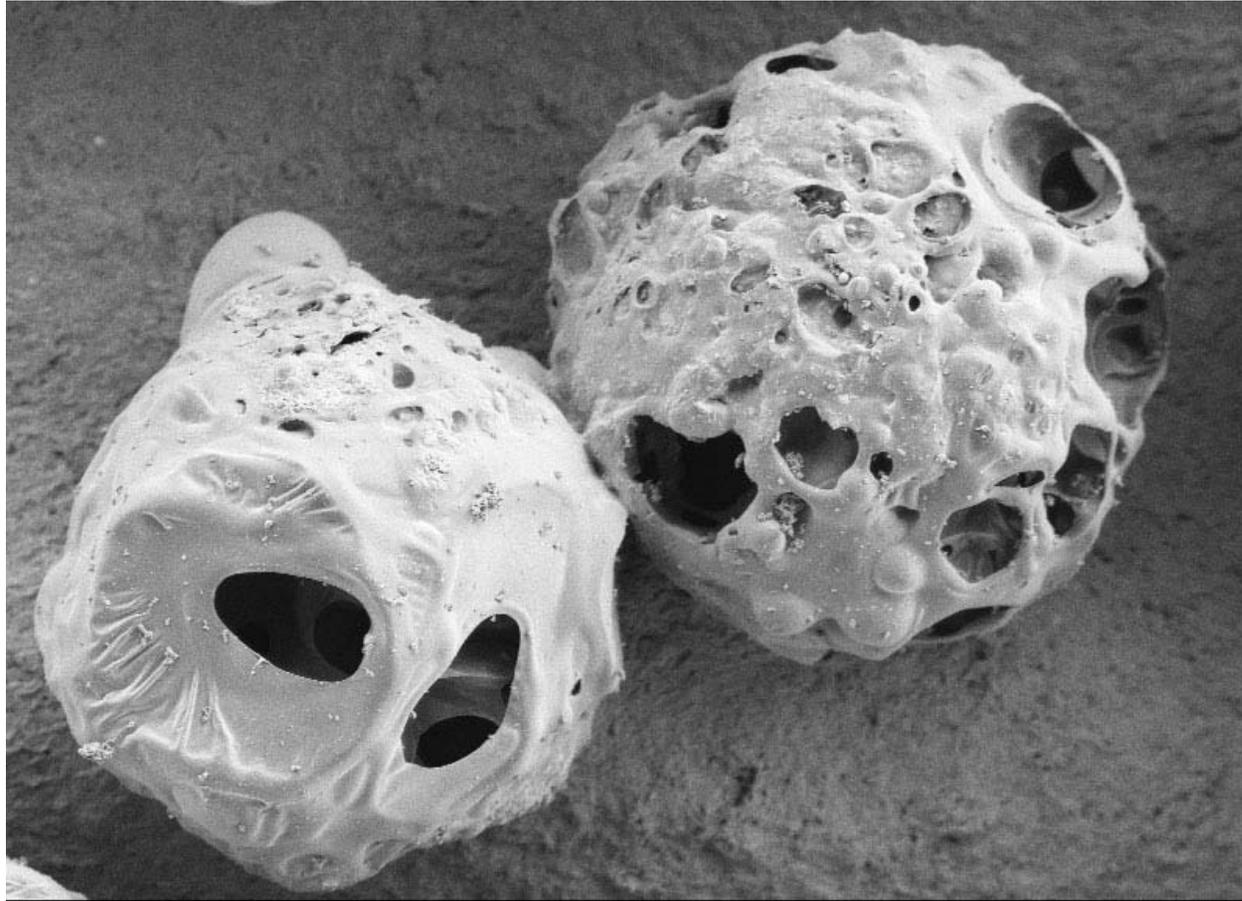
PRB Coal Char

10 bar, O/Coal 200%

30 bar, O/Coal 154%



Pittsburgh, 30 atm., O/C: 9.5%



= 1.00 K X
20µm
|-----|

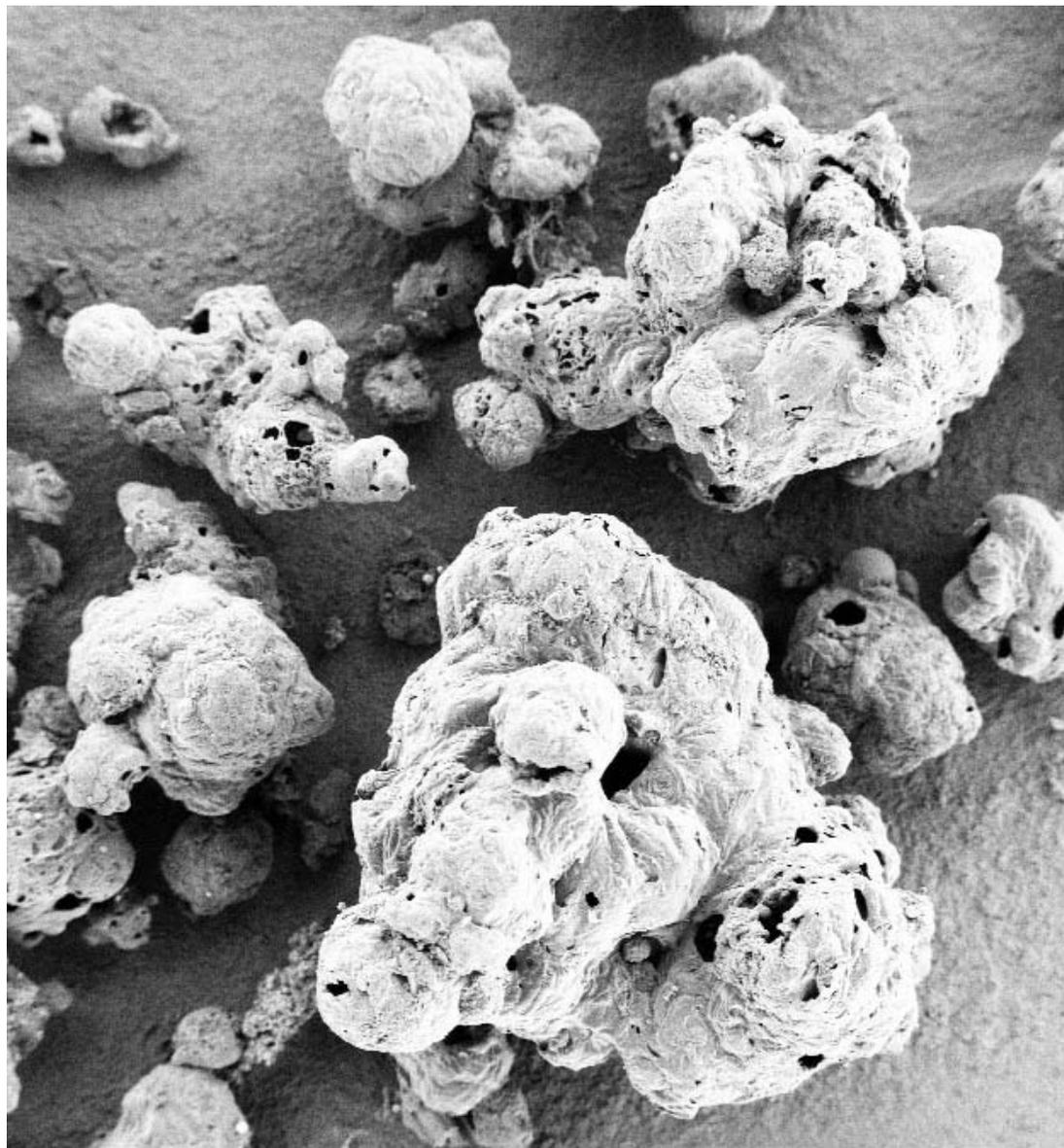
EHT = 3.03 kV
WD = 11 mm

Signal A = VPSE
Photo No. = 953

Date :25 M
Time :20:0

*Agglomeration
and coalescence*

Illinois #6, 2 atm.
O/C: 160%

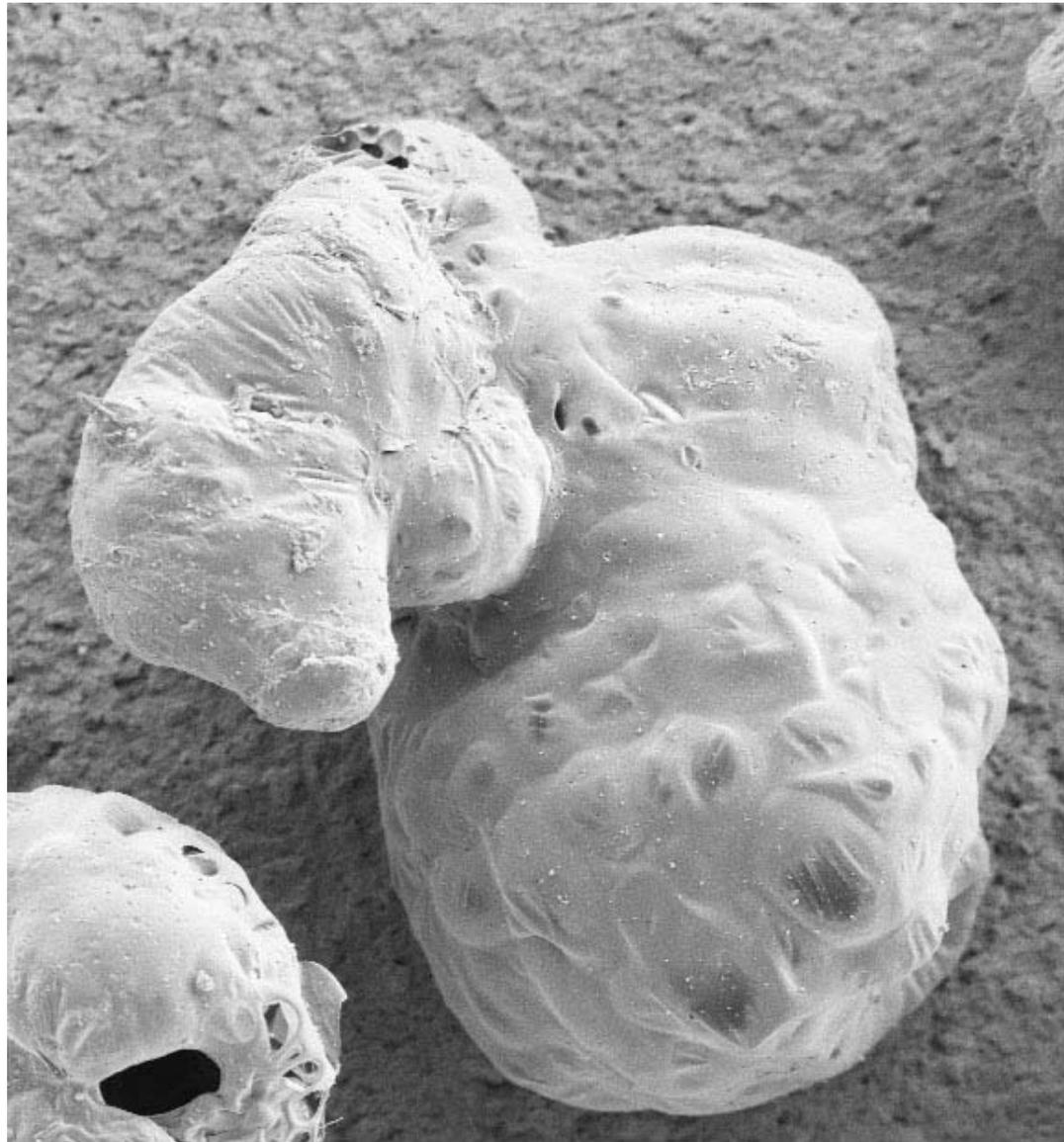


X 200μm
|-----|

EHT = 3.07 kV
WD = 10 mm

Signal A = VPSE
Photo No. = 568

Pittsburgh,
30 atm.
O/C: 48.6%

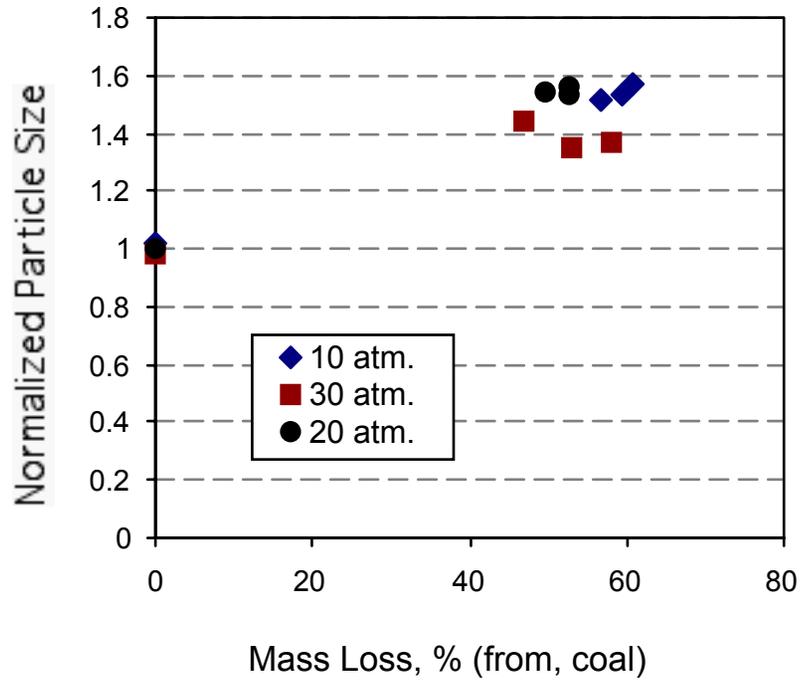


20 μ m
|—|

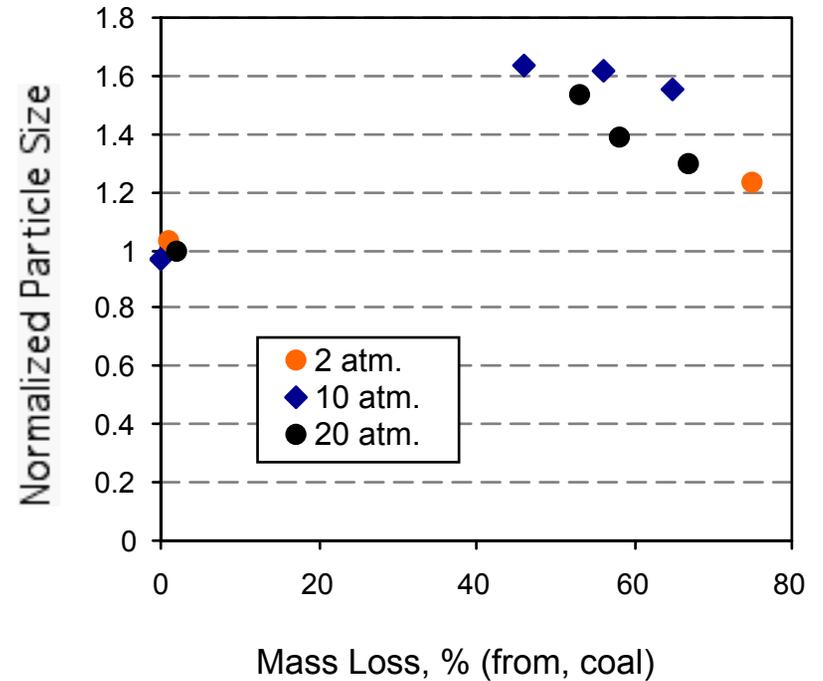
EHT = 3.03 kV
WD = 11 mm

Signal A = VPS
Photo No. = 946

Quantitative Swelling Data from For High Pressure Chars



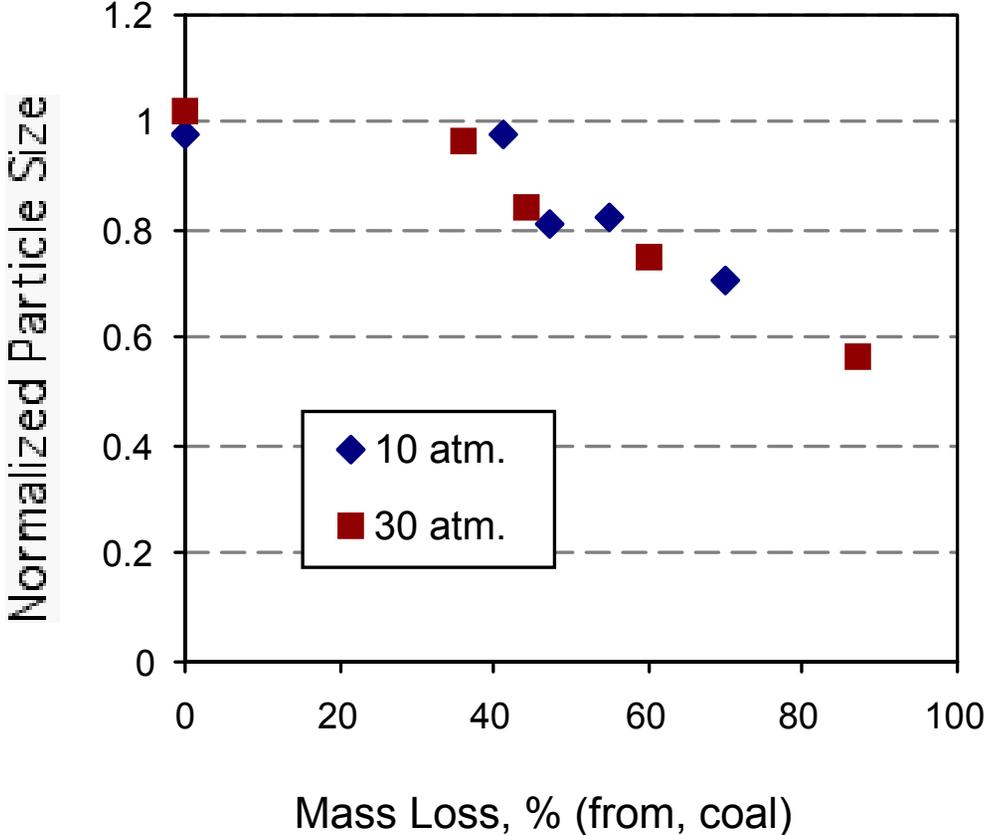
Pittsburgh #8



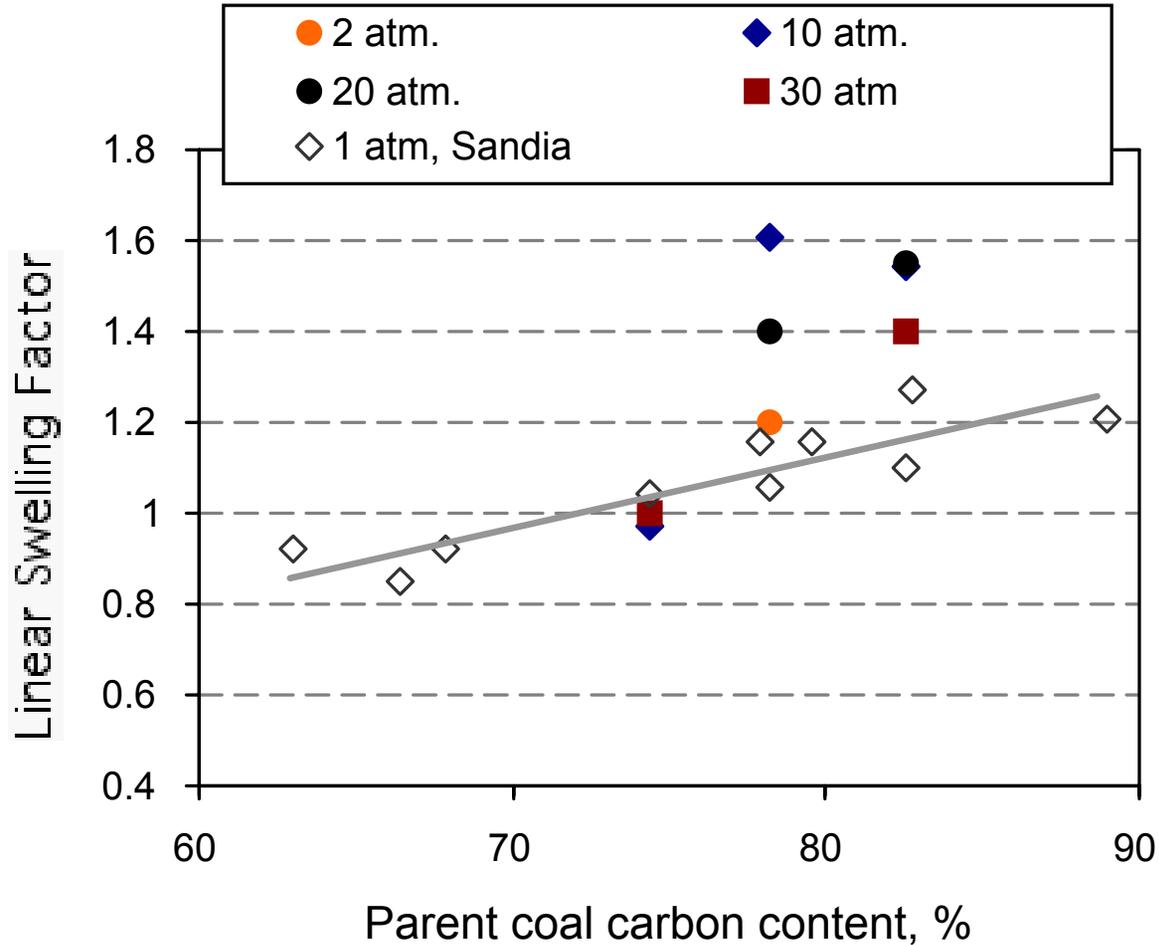
Illinois #6

Quantitive Swelling Data for High Pressure Chars

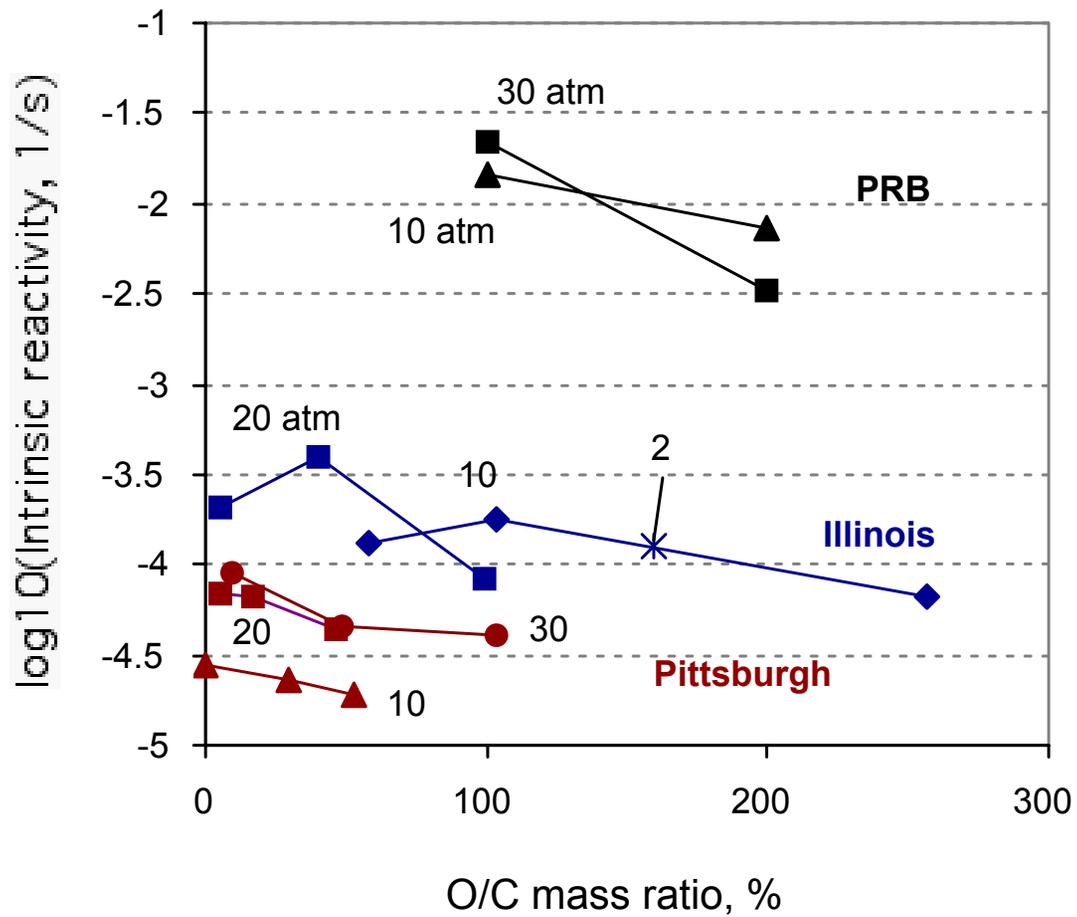
PRB coal



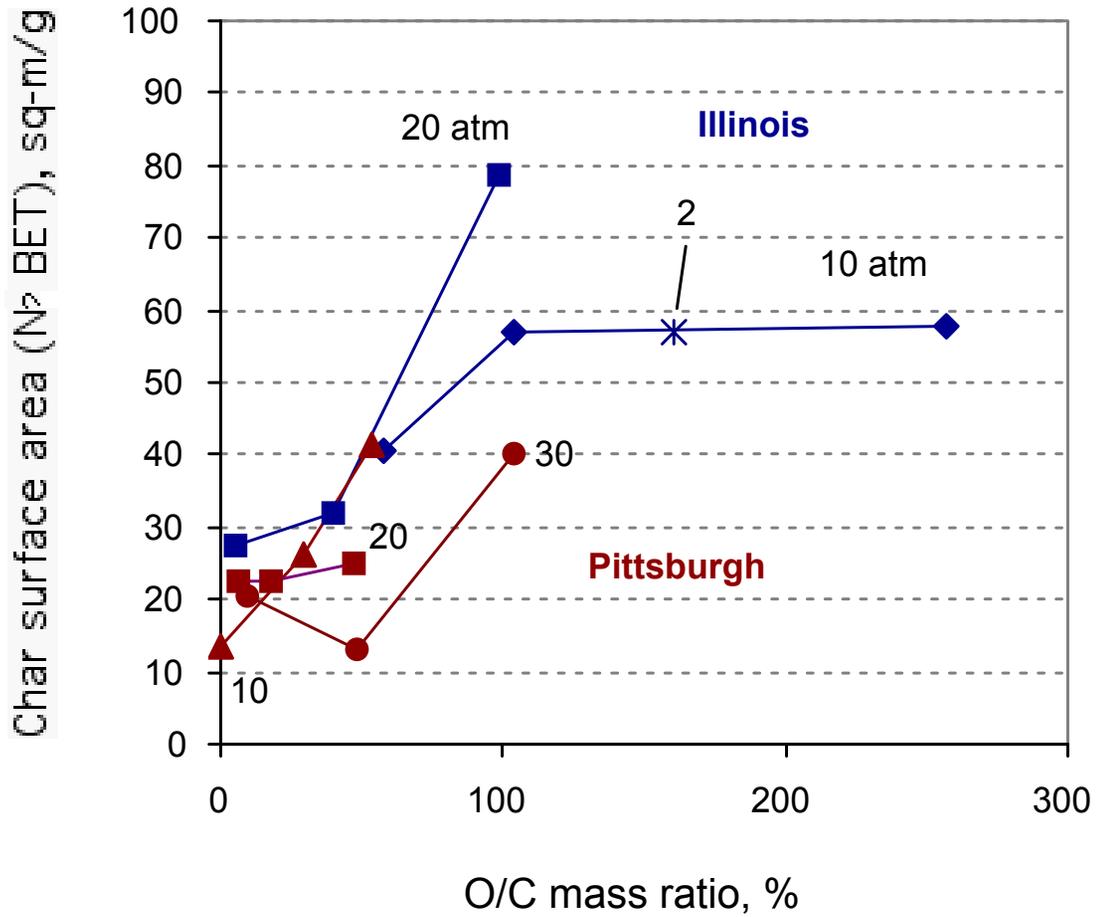
Summary of High Pressure Swelling Data and Comparison to 1 atm Flow Reactor Data (Sandia)



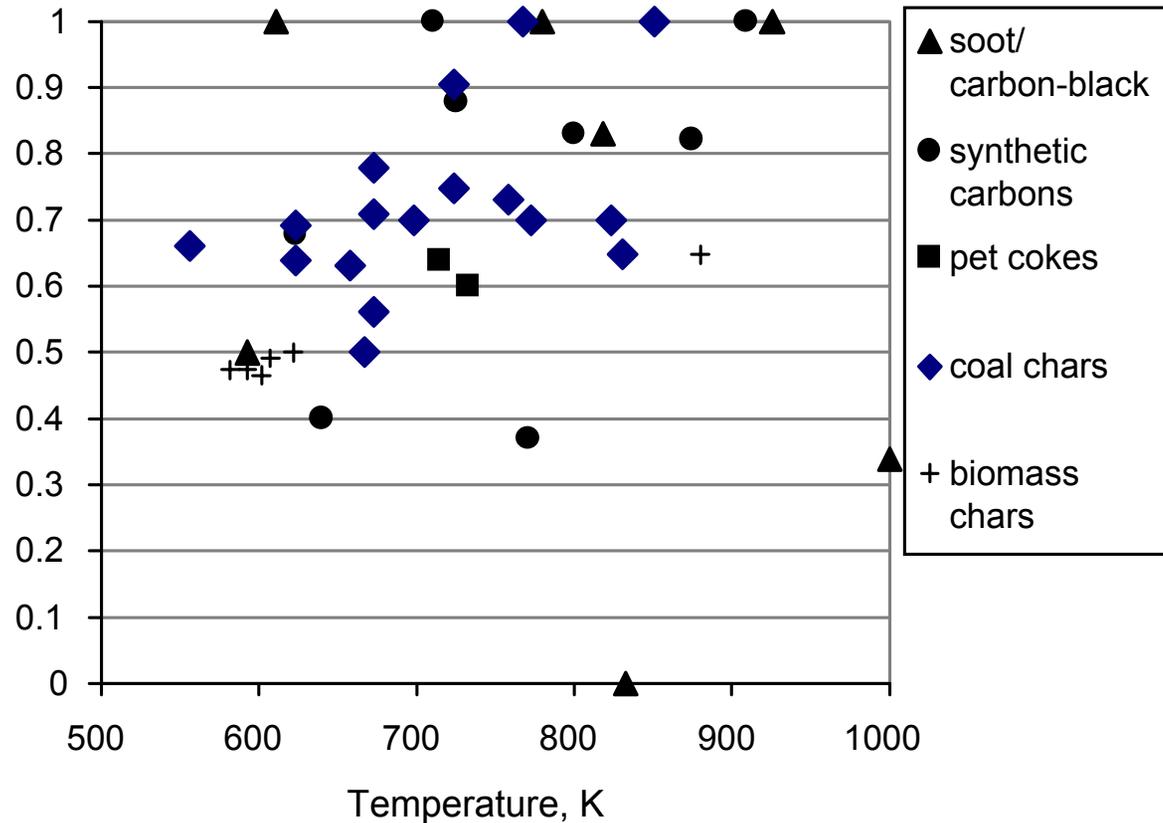
Intrinsic Reactivities of High Pressure Chars



Total Surface Areas of High Pressure Chars



Carbon/Oxygen Reaction: Review of Measured Reaction Orders in Intrinsic Regime



The observed high, fractional reaction orders are not consistent with the simple 2-step mechanistic kinetic models in current use

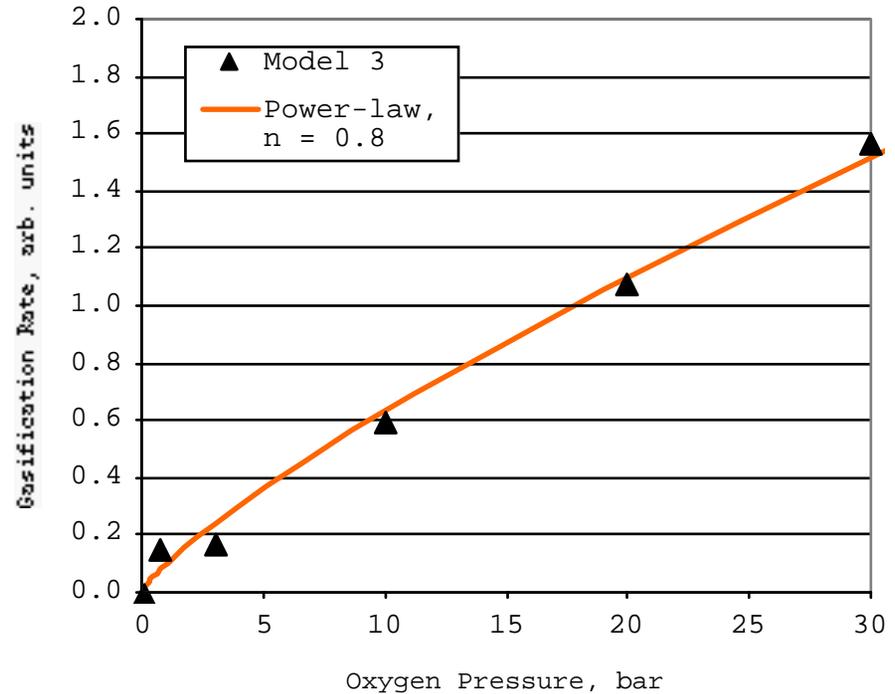
High Pressure Combustion Kinetics

Proposed 3-step semi-global mechanism



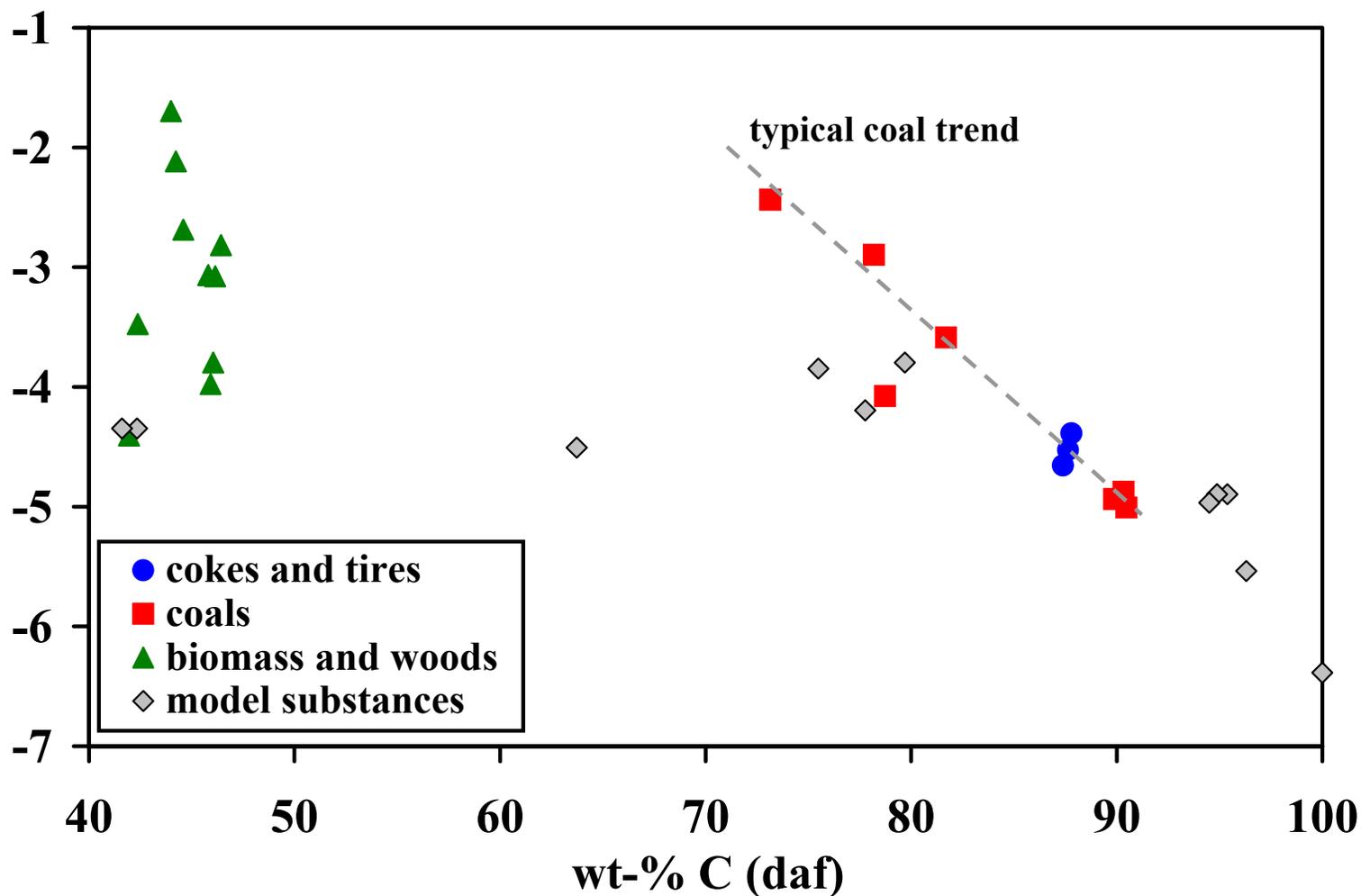
$$r_{\text{gas}} = \frac{k_1 k_2 P_{\text{O}_2}^2 + k_1 k_3 P_{\text{O}_2}}{k_1 P_{\text{O}_2} + k_3/2}$$

$$\text{CO}/\text{CO}_2 = \frac{k_3}{k_2 P_{\text{O}_2}}$$



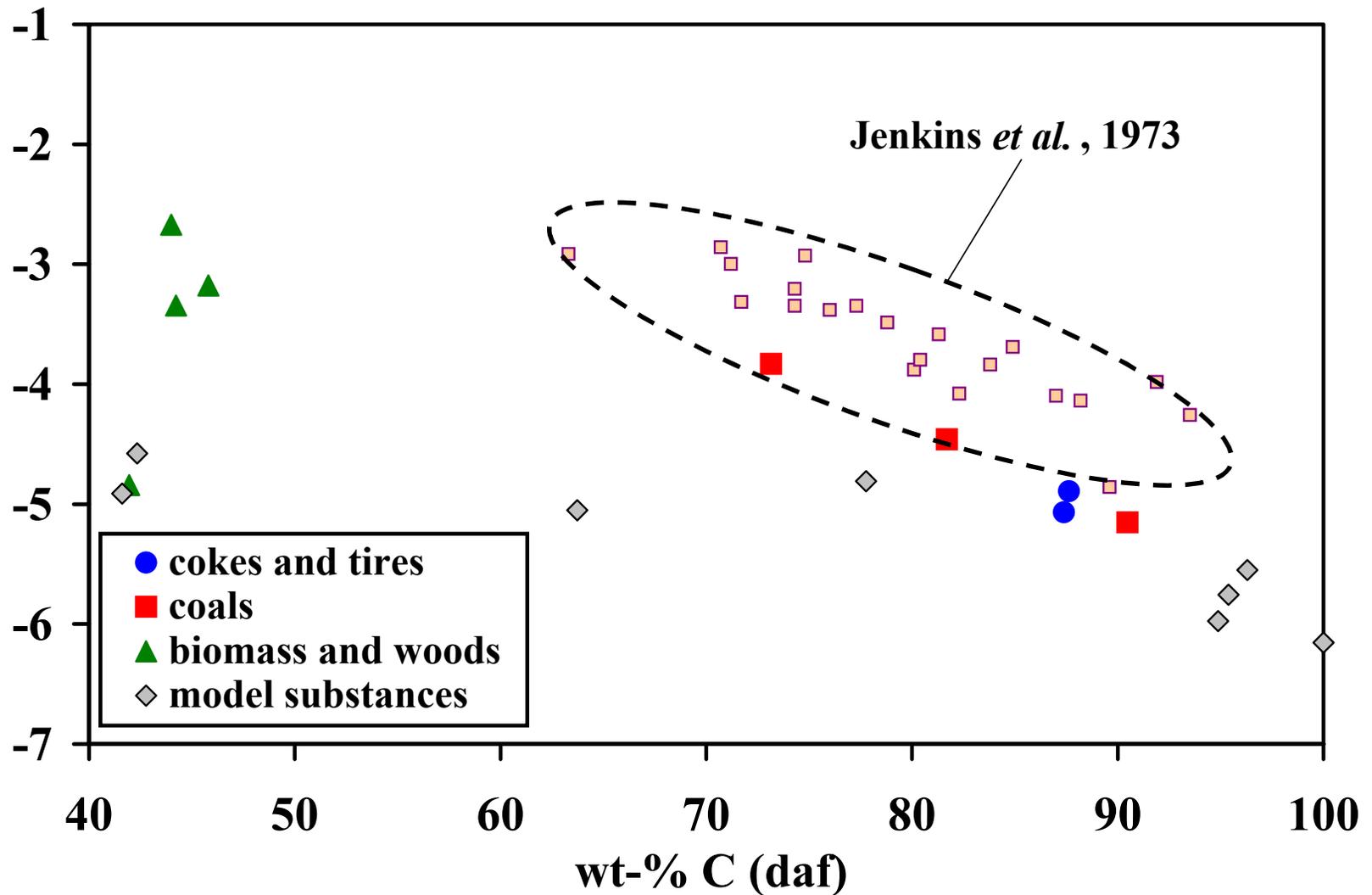
Project on Predicting Reactivities of Diverse Solid Fuel Chars

$\log_{10} R$ [sec⁻¹]

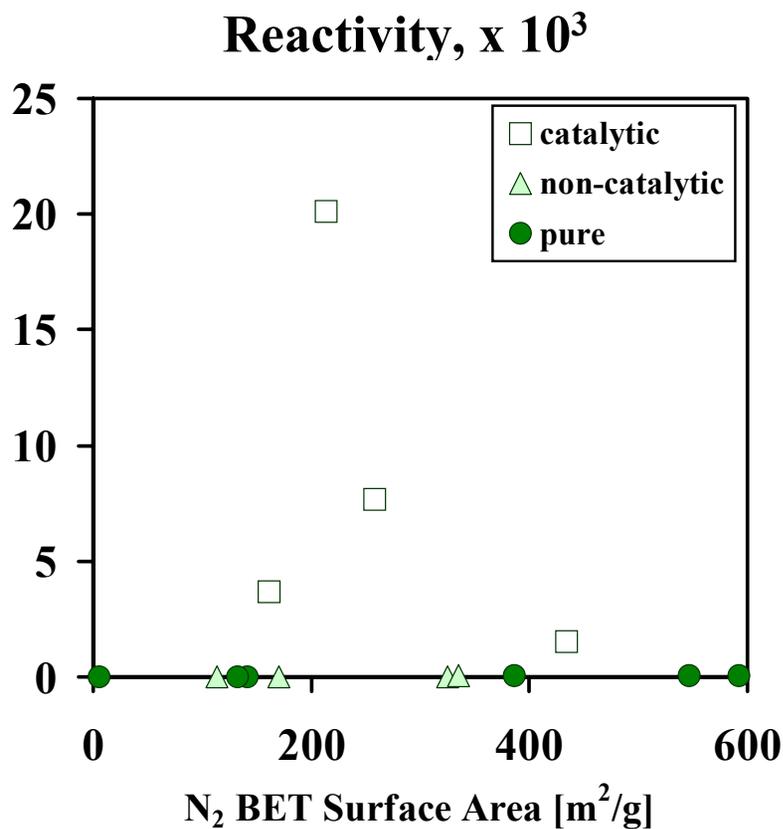


Reactivity of 1000°C Chars

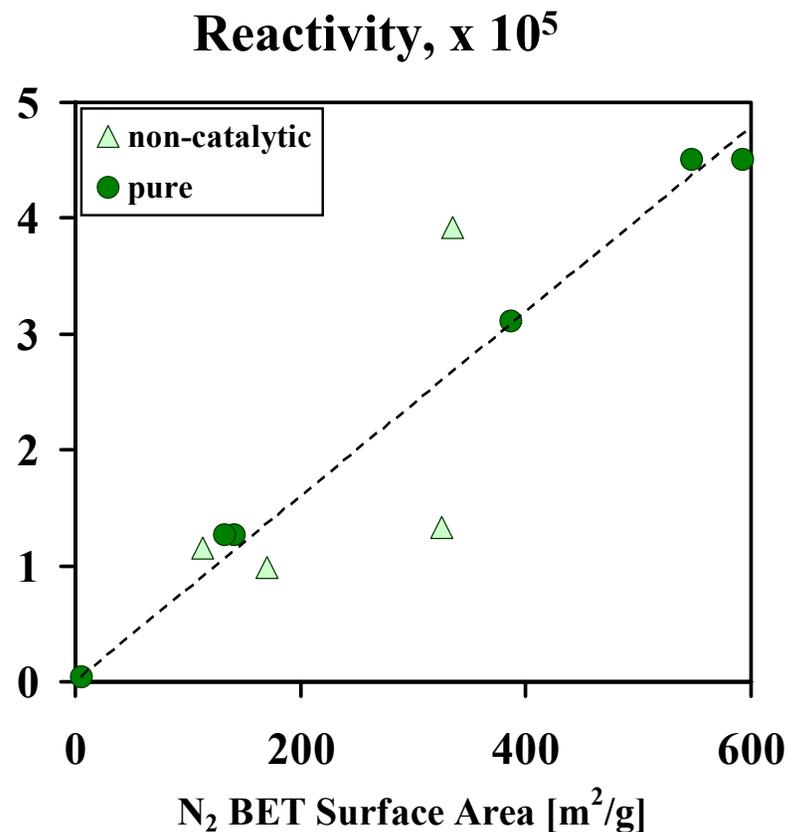
$\log_{10} R$ [sec⁻¹]



Total Char Surface Area



***POOR correlation:
entire sample bank***



***STRONG correlation:
non-catalytic mat'ls***

Model Development

Hybrid chemical/statistical approach

Two independent, parallel, non-catalytic and catalytic components are assumed:

$$R_{700^{\circ}\text{C}} = R_{\text{carb}} + R_{\text{cat}}$$

R_{carb} = function of:

%C (parent fuel)

or

char surface area

R_{cat} = function of:

concentration
and

dispersion

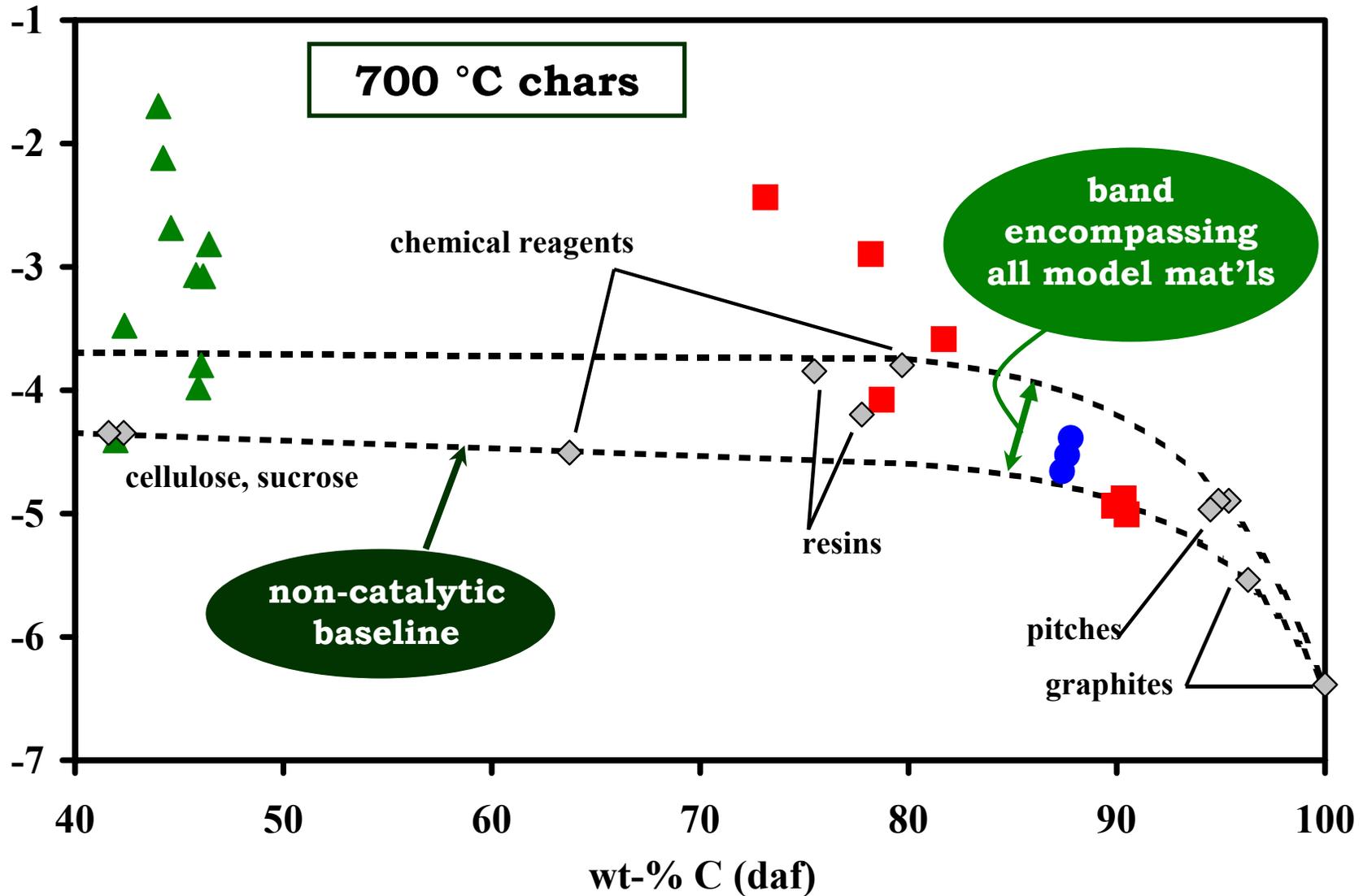
of

Group I, II, and
transition metals*

*in this data set: K, Ca+Mg, V

Non-Catalytic Baseline

$\log_{10} R$ [sec⁻¹]



Catalyst Dispersion

Catalyst activity depends strongly on grain size [Radovic *et al.*, 1983; Cope *et al.*, 1994; numerous heterogeneous catalysis studies]

Bulk granular mineral matter in coals has low catalytic activity [Tomita *et al.*, 1977]

in parent materials

- exchanged cations
- soluble salts
- organometalics w/ essential biofunction
-
- mineral grains
- granular additives
- soil



in chars

- nanophase particles (highly active)
-
- bulk inorganic matter, $d > 1\mu\text{m}$ (low activity)

“nanophase dispersion”

“granular dispersion”

coals

mixed nano- and granular dispersion

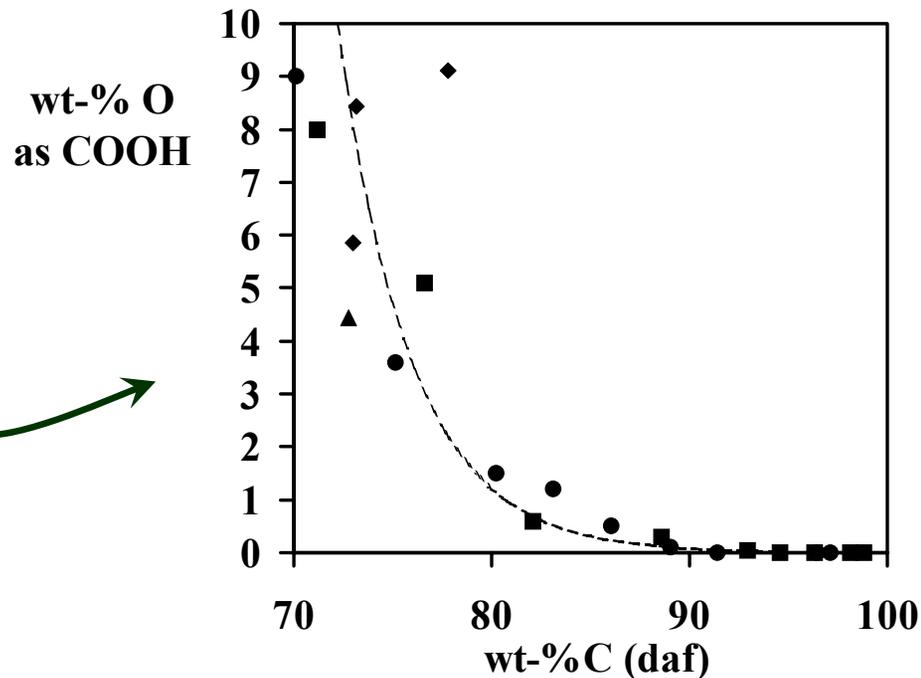
nanodispersed fraction determined by comparing concentration of ion-exchange (carboxylic) sites to catalyst loading

biomass

mixed nano- and granular dispersion

K (dominant) and Ca: primarily in soluble or ion-exchangeable forms [Jenkins *et al.*, 1998], except bagasse, which has been washed during processing.

Fuel-Specific Dispersion Rules



tires

granular inorganic impurities

cokes

V is nano-dispersed in porphyrins

Hybrid Approach Result

Reactivity, R

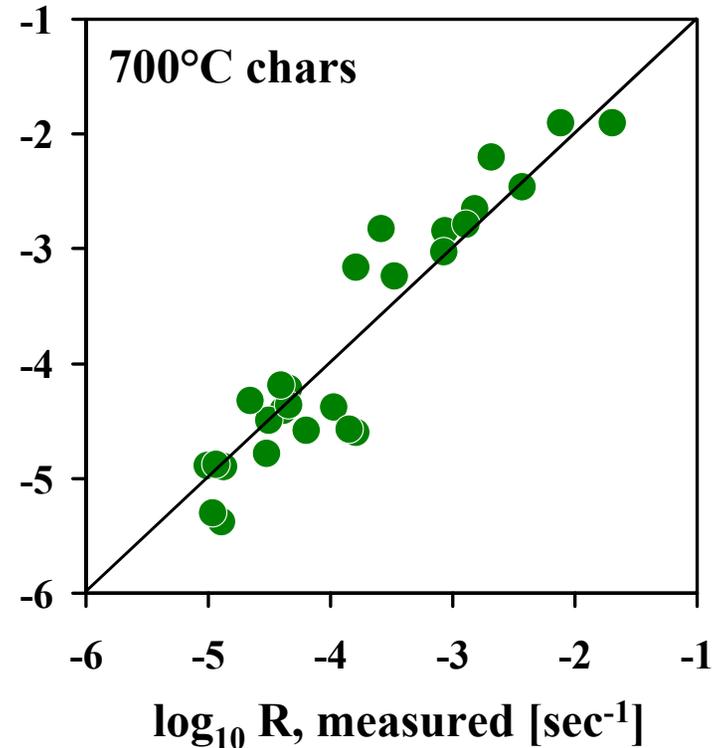
=

$R_{\text{carb}} = \text{fxn}(\text{wt-\% C of precursor})$

+

$$\begin{aligned} R_{\text{cat}} = & 7.9 \cdot 10^{-7} (K_{\text{nano}}) \\ & + 1.3 \cdot 10^{-7} (\text{Ca}_{\text{nano}} + \text{Mg}_{\text{nano}}) \\ & + 3.1 \cdot 10^{-8} (V_{\text{nano}}) \end{aligned}$$

$\log_{10} R,$
model
[sec⁻¹]



Most reactivity variation explained through 4 precursor properties:

$K_{\text{nano}}, (\text{Ca} + \text{Mg})_{\text{nano}}, \text{wt-\% C}, V_{\text{nano}}$

(in order of decreasing importance)

Reactivities of Diverse Solid Fuels: Conclusions

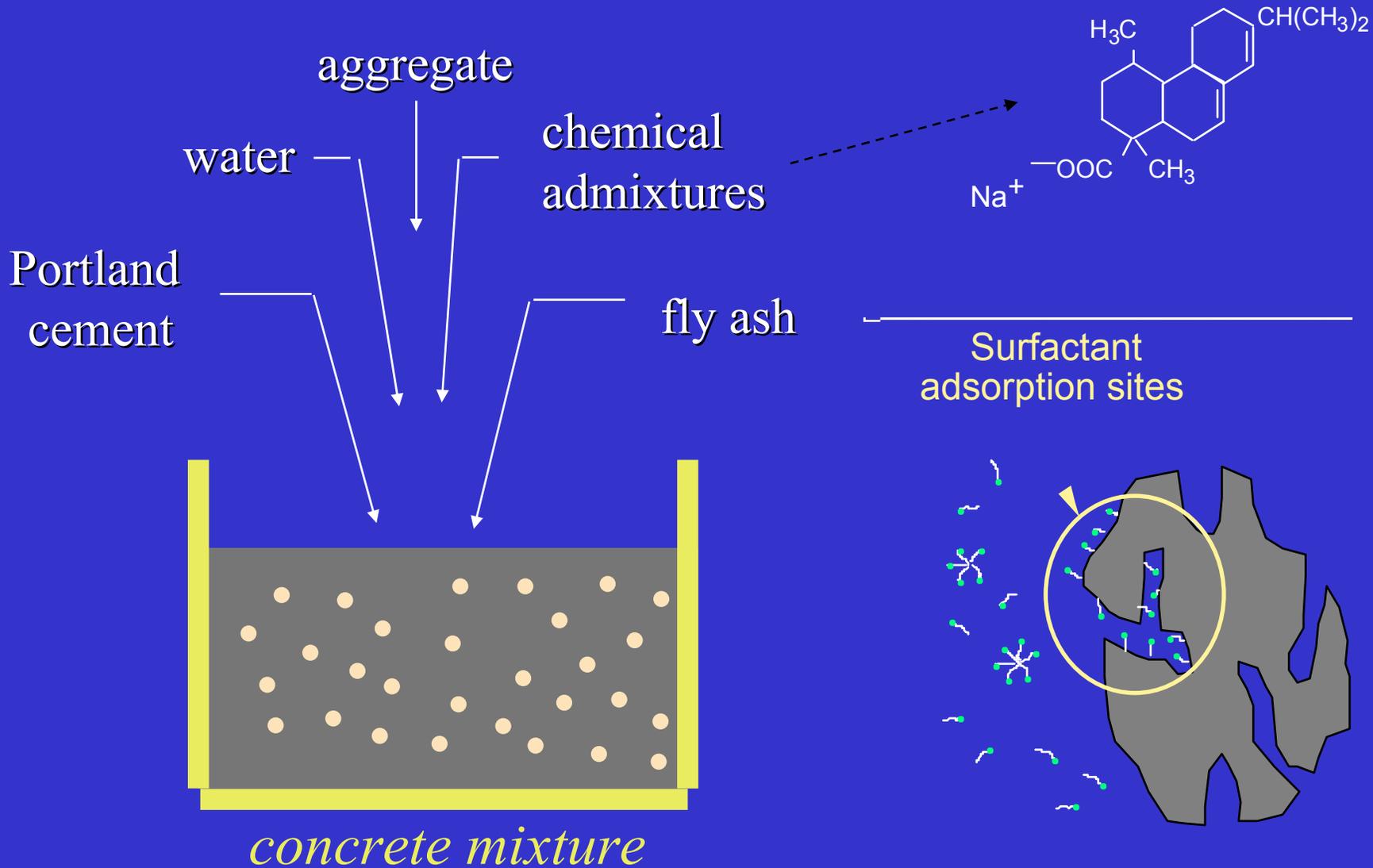
For coals, reactivity correlates well with organic composition (C,H,O,N,S), but the trend is NOT evident for solid fuels of < 80% C, daf (most practical fuels).

For 700°C chars, catalysis is the dominant factor determining reactivity trends (in agreement with most demineralization studies).

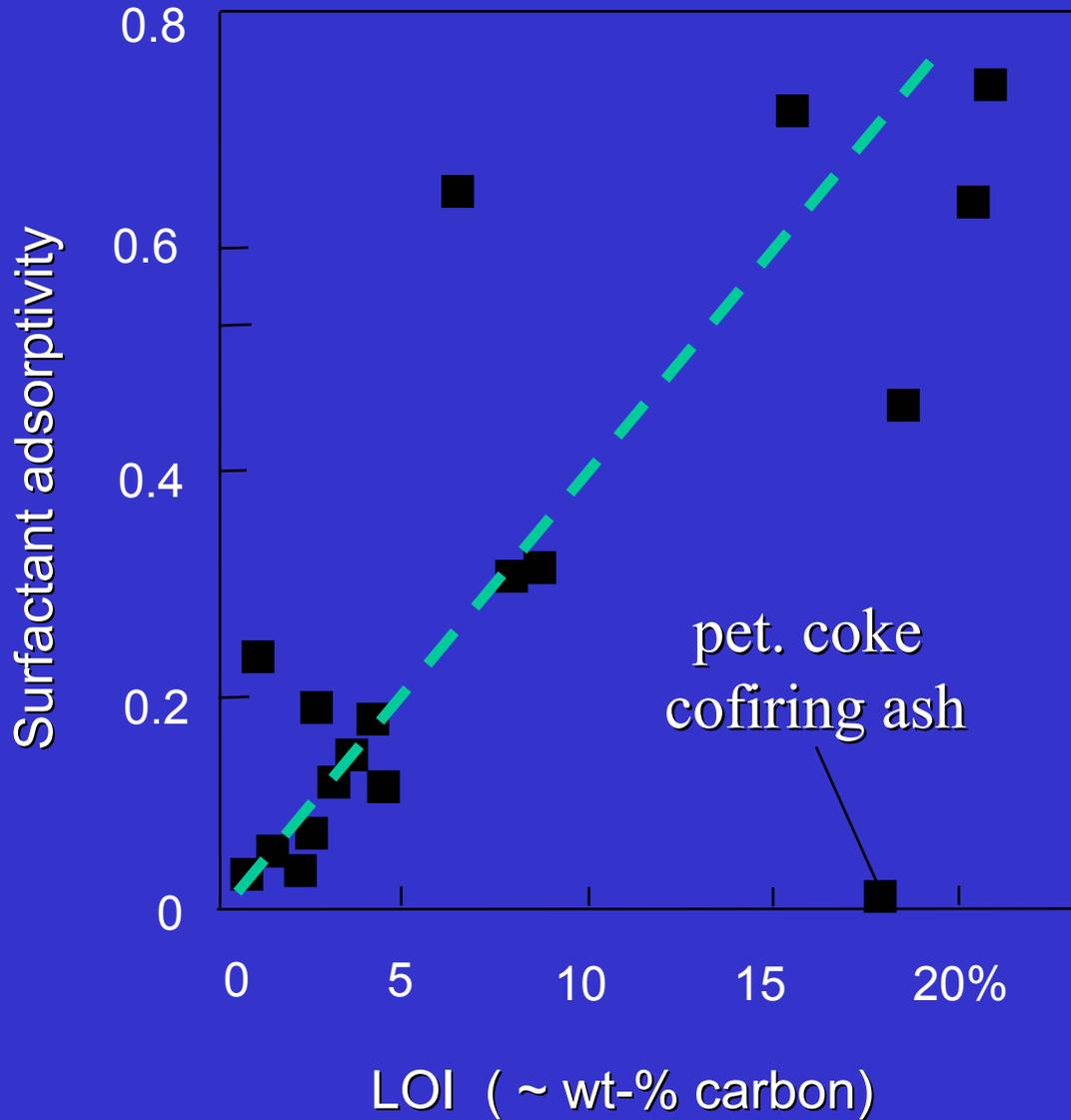
Sensitivity studies (according to model coefficients) suggest that virtually no natural materials can be safely assumed to be non-catalytic. [K_{nano} must be < 44 ppm; $(\text{Ca}+\text{Mg})_{\text{nano}}$ < 270 ppm]

Crude estimation of reactivity is possible based on parent fuel characterization alone, *if* the model incorporates literature information on the form and dispersion of inorganic matter.

Air Entrainment in Fly Ash Concrete

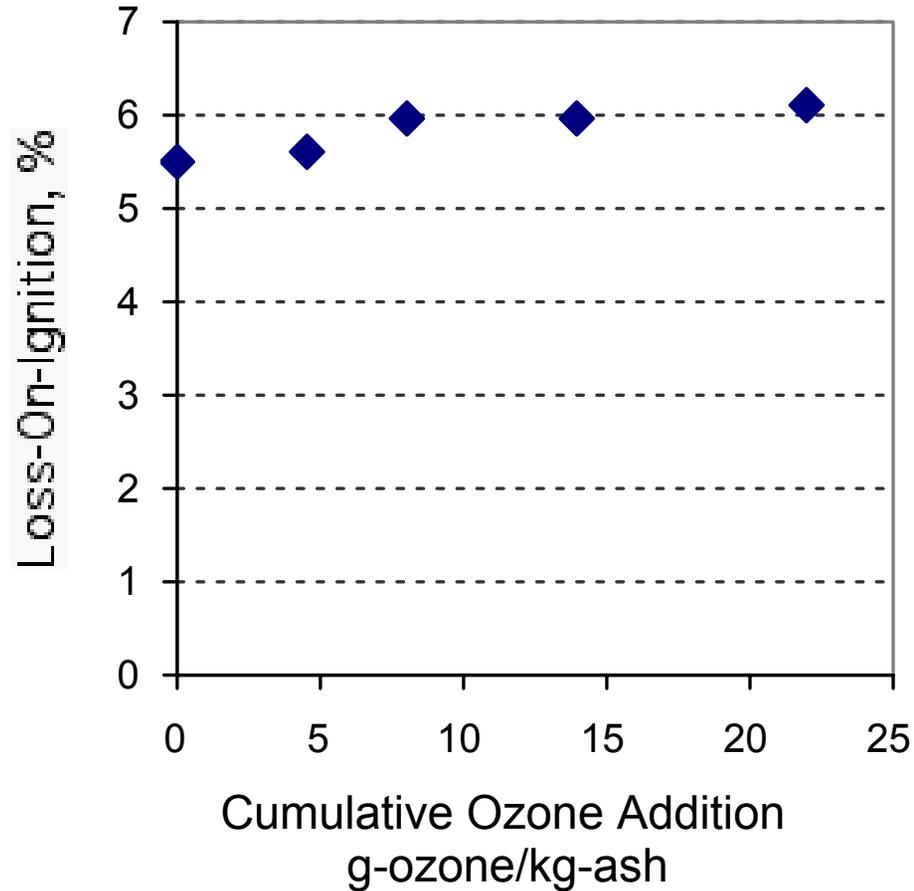


[Freeman, et al., 1996; Smith et al., 1998]



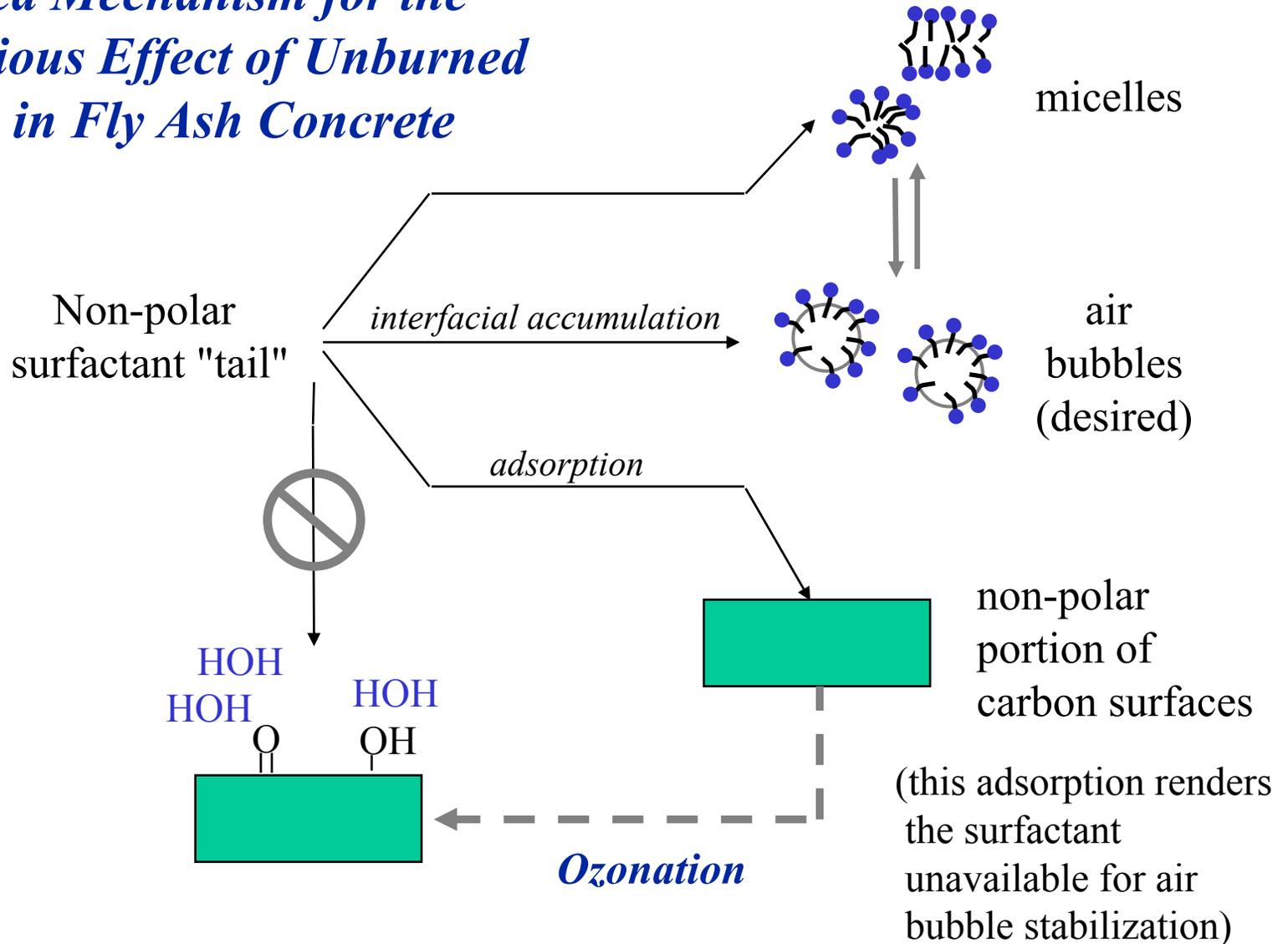
- surfactant adsorptivity varies widely
- variation at constant LOI is significant
- behavior related to carbon *properties*

Effect of Ozonation on Carbon Content



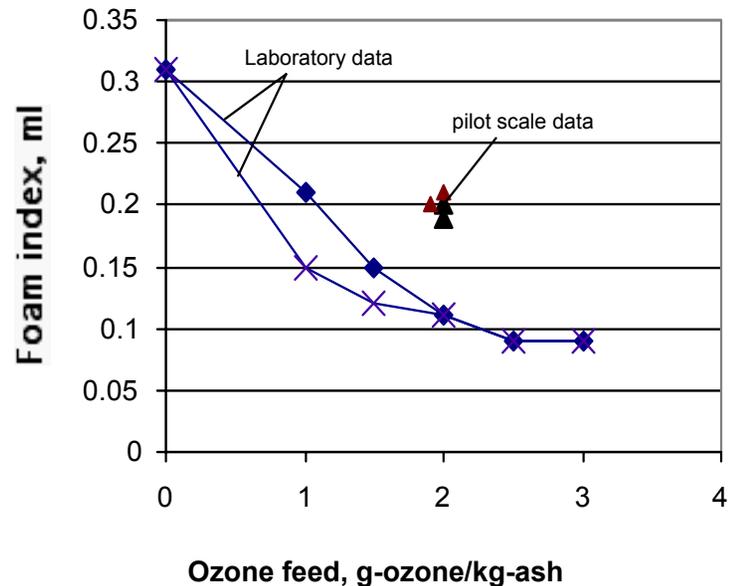
The major effect is *surface* oxidation, not carbon consumption

Proposed Mechanism for the Deleterious Effect of Unburned Carbon in Fly Ash Concrete



Development and Scale-up of Ash Ozonation Process

A team of organizations has been assembled to pursue the design, scale-up and commercialization of Brown's patented fly ash ozonation technology. The team includes: PCI-Wedeco, PP&L (power generating utility), Fuller Bulk Handling, EPRI, Brown, and EES for support and project management. along with funding from the Dept. of Energy, National Energy Technology Laboratory



First generation pilot plant at PCI-Wedeco, West Caldwell N.J., the world's leading manufacturer of ozone generators. **Left:** portion of the pilot plant; **Right:** early results.

ACKNOWLEDGMENTS

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